

for Aeronautics

MAILED

JUN 18 1938

JUN 22 1938

To: *Library L. M. A. L.*

TECHNICAL NOTES

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

No. 652

4.1
4.7.2
9.2

TABLES OF STIFFNESS AND CARRY-OVER FACTOR

FOR STRUCTURAL MEMBERS UNDER AXIAL LOAD

By Eugene E. Lundquist and W. D. Kroll
Langley Memorial Aeronautical Laboratory

FILE COPY

To be returned to
the files of the Langley
Memorial Aeronautical
Laboratory.

Washington
June 1938



3 1176 01425 6623

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE NO. 652

TABLES OF STIFFNESS AND CARRY-OVER FACTOR FOR STRUCTURAL MEMBERS UNDER AXIAL LOAD

By Eugene E. Lundquist and W. D. Kroll

SUMMARY

Tables of stiffness and carry-over factor are presented for members in which the cross section and axial load do not vary along the length of the member. These tables are of use in solving problems in the stability of structural members under axial load as well as in applications of the Cross method of moment distribution when the effects of axial load in the members are considered. The interval between successive values of the argument is small enough to make interpolation unnecessary in engineering calculations.

INTRODUCTION

The method of moment distribution developed by Hardy Cross (reference 1) can frequently be used to advantage in the stress analysis of continuous beams, continuous frames, and rigid joint trusses, some cases of which occur in aeronautical structures. In reference 2 James summarized the principles of the Cross method and extended it to show how the effects of axial load in the members may be considered in a moment-distribution analysis. In reference 3 the Cross method was further extended to show how the principles of moment distribution may be used to solve problems in the stability of structural members under axial load.

In the stability calculations as well as in a moment-distribution analysis where the effects of axial load are considered, it is desirable to have tables giving the stiffness and carry-over factor as a function of the axial load and properties of the member. Such a set of tables is presented in this paper.

The tables apply to members for which the cross section and axial load do not vary along the length of the member. The interval between successive values of the argument was made so small that no interpolation will be necessary when the tables are used in engineering calculations.

DEFINITIONS AND SYMBOLS

The following definitions of stiffness and carry-over factor are the same as those given in reference 3, which parallel the definitions given in references 1 and 2 with some changes in wording.

Stiffness

If a member is on unyielding supports at each end, the moment at one end necessary to produce a rotation of one-fourth radian of that end is called the "stiffness." The stiffness of a member will depend upon the amount of restraint at the far end. In the derivation of the criterion for stability as given in reference 3, three types of restraint at the far end are considered. The symbols used to designate the stiffness for the different types of restraint are:

S, far end fixed.

S', far end elastically restrained.

S'', far end pinned.

The stiffness of a member computed according to the foregoing definition is one-fourth that computed according to the definition given in references 1 and 2. In the Cross method the relative stiffness of the members is of importance and not the absolute value. The foregoing definition was selected so that the stiffness of a member of constant cross section with no axial load and fixed at the far end would be \bar{EI}/L instead of $4\bar{EI}/L$.

Carry-Over Factor

If a member is on unyielding supports at each end and

a moment is applied at the near end, the ratio of the moment developed at the far end to the moment applied at the near end is called the "carry-over factor." As in the case of stiffness, the carry-over factor will depend upon the degree of restraint at the far end of the member. The symbols used to designate the carry-over factor for the different types of restraint are:

C, far end fixed.

C', far end elastically restrained.

C" = 0, far end pinned.

Sign Convention

The sign convention used in this report is the same as that used in references 2 and 3. A clockwise moment acting on the end of a member is positive. A counter-clockwise moment acting on a joint is positive. An external moment applied at a joint is considered to act on the joint.

Symbols

E, modulus of elasticity.

\bar{E} , effective modulus of elasticity.

I, moment of inertia of cross section of member about a centroidal axis normal to the plane of bending.

L, length of member.

P, axial load in member (absolute value).

$$\alpha = 6 \frac{\frac{L}{j} \csc \frac{L}{j} - 1}{\left(\frac{L}{j}\right)^2}$$

$$\beta = 3 \frac{1 - \frac{L}{j} \cot \frac{L}{j}}{\left(\frac{L}{j}\right)^2}$$

For compression members

$$\left. \begin{aligned}
 \alpha &= 6 \frac{\frac{L}{j} \operatorname{csch} \frac{L}{j} - 1}{-\left(\frac{L}{j}\right)^2} \\
 \beta &= 3 \frac{1 - \frac{L}{j} \coth \frac{L}{j}}{-\left(\frac{L}{j}\right)^2}
 \end{aligned} \right\} \text{For tension members}$$

$$j = \sqrt{\frac{EI}{P}}$$

$$\frac{L}{j} = L \sqrt{\frac{P}{EI}}$$

$$\left(\frac{L}{j}\right)_{\text{eff}} = L \sqrt{\frac{P}{EI}}$$

Effective values of α and β are obtained by substitution of $(L/j)_{\text{eff}}$ for L/j .

FORMULAS USED IN CALCULATION OF TABLES

In tables I and II for compression and tension, respectively, the far end of the member is considered as either pinned or fixed. The stiffness and carry-over factor that applies when the far end is elastically restrained is expressed in terms of these quantities by formulas given in reference 3.

The argument in tables I and II is $(L/j)_{\text{eff}}$. In the elastic range $\bar{E} = E$ and $(L/j)_{\text{eff}} = (L/j)$. Above the elastic range, however, it is necessary to use a reduced modulus \bar{E} , which is called the "effective modulus." In reference 3 it is shown how the effective modulus can be

obtained from the accepted column formula for the material comprising the member.

The second, third, and fourth columns in tables I and II were computed by means of the following formulas:

$$c = \frac{\alpha}{2\beta} \quad (1)$$

$$\frac{s''}{\left(\frac{EI}{L}\right)} = \frac{3}{4\beta} \quad (2)$$

$$\frac{s}{\left(\frac{EI}{L}\right)} = \frac{s''}{\left(\frac{EI}{L}\right)} \left[\frac{1}{1 - c^2} \right] \quad (3)$$

These equations were first presented by James in reference 2 except that the more general form of equation (3) is taken from reference 3.

The last two columns in tables I and II were obtained from the preceding columns as indicated by their headings. These columns are included because of their convenience in stability calculations (reference 3).

ACCURACY OF TABLES

The tables of reference 4 were used in the preparation of tables I and II. All calculations were made using eight significant figures. Equations (1), (2), and (3) were used in the form and order given to calculate the second, third, and fourth columns. The fifth column was obtained by squaring the second column. The sixth column was obtained by squaring the fourth column and multiplying by the fifth column. The last column was therefore made to depend upon all preceding columns. All values were then tabulated to six significant figures and the differences for the last

column were studied; in some cases as much as the fourth difference was used. An independent check was also made for a series of values throughout the tables as well as where errors were suggested by irregular differences. In each case where errors were suspected, they were traced to the tables of reference 4.

Langley Memorial Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., May 12, 1938.

REFERENCES

1. Cross, Hardy: Analysis of Continuous Frames by Distributing Fixed-End Moments. A.S.C.E. Trans., vol. 96, 1932, pp. 1-10.
2. James, Benjamin Wylie: Principal Effects of Axial Load on Moment-Distribution Analysis of Rigid Structures. T.N. No. 534, N.A.C.A., 1935.
3. Lundquist, Eugene E.: Stability of Structural Members under Axial Load. T.N. No. 617, N.A.C.A., 1937.
4. Hayashi, Keiichi: Sieben- und mehrstellige Tafeln der Kresi- und Hyperbelfunktionen und deren Producte sowie der Gammafunktion. Julius Springer (Berlin), 1926.

TABLE I
COMPRESSION

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
0	0.500000	0.750000	1.000000	0.250000	0.250000
.1	.500243	.749505	.999664	.250243	.250075
.2	.501001	.747996	.998663	.251002	.250332
.3	.502260	.745488	.996996	.252265	.250752
.4	.504034	.741963	.994656	.254050	.251342
.5	.506333	.737410	.991639	.256373	.252104
.6	.509173	.731812	.987943	.259257	.253043
.7	.512572	.725149	.983561	.262780	.254163
.8	.516555	.717398	.978486	.266829	.255471
.9	.521146	.708528	.972709	.271593	.256971
1.0	.526380	.698505	.966221	.277075	.258673
1.01	.526940	.697438	.965532	.277665	.258854
1.02	.527506	.696358	.964837	.278263	.259038
1.03	.528080	.695267	.964134	.278869	.259224
1.04	.528661	.694164	.963424	.279482	.259411
1.05	.529249	.693049	.962707	.280104	.259602
1.06	.529843	.691921	.961982	.280734	.259794
1.07	.530445	.690782	.961250	.281372	.259988
1.08	.531054	.689630	.960511	.282018	.260185
1.09	.531669	.688466	.959764	.282672	.260383
1.10	.532293	.687289	.959011	.283336	.260584
1.11	.532923	.686100	.958249	.284007	.260787
1.12	.533561	.684899	.957481	.284687	.260992
1.13	.534205	.683685	.956705	.285375	.261200
1.14	.534855	.682459	.955922	.286073	.261410
1.15	.535517	.681220	.955131	.286779	.261621
1.16	.536185	.679968	.954333	.287494	.261836
1.17	.536859	.678704	.953527	.288218	.262052
1.18	.537542	.677427	.952715	.288951	.262271
1.19	.538232	.676137	.951894	.289693	.262492
1.20	.538929	.674834	.951066	.290445	.262715
1.21	.539635	.673518	.950231	.291206	.262941
1.22	.540348	.672190	.949388	.291976	.263169
1.23	.541069	.670848	.948538	.292755	.263399
1.24	.541798	.669493	.947680	.293545	.263632
1.25	.542535	.668125	.946814	.294344	.263867
1.26	.543279	.666744	.945941	.295153	.264104
1.27	.544033	.665350	.945061	.295971	.264344
1.28	.544794	.663942	.944173	.296800	.264586
1.29	.545563	.662521	.943277	.297639	.264830
1.30	.546341	.661086	.942374	.298488	.265078
1.31	.547127	.659638	.941462	.299347	.265327
1.32	.547921	.658176	.940544	.300217	.265579
1.33	.548724	.656701	.939618	.301098	.265833
1.34	.549535	.655212	.938683	.301989	.266090
1.35	.550355	.653707	.937742	.302890	.266350
1.36	.551183	.652192	.936792	.303803	.266611
1.37	.552021	.650661	.935835	.304727	.266876
1.38	.552867	.649116	.934870	.305662	.267143
1.39	.553722	.647557	.933897	.306608	.267412
1.40	.554585	.645984	.932917	.307565	.267684

TABLE I (Continued)
COMPRESSION

$\left(\frac{L}{j}\right)_{eff}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
1.41	.355458	.644597	.931928	.308554	.267959
1.42	.356340	.642795	.930932	.309575	.268236
1.43	.357231	.641179	.929928	.310507	.268516
1.44	.358132	.639549	.928916	.311511	.268798
1.45	.359041	.637903	.927896	.312527	.269084
1.46	.359961	.636244	.926869	.313556	.269371
1.47	.360889	.634569	.925833	.314597	.269662
1.48	.361827	.632880	.924790	.315650	.269958
1.49	.362775	.631176	.923738	.316716	.270251
1.50	.363733	.629457	.922679	.317794	.270550
1.51	.364700	.627723	.921611	.318886	.270851
1.52	.365677	.625973	.920536	.319990	.271156
1.53	.366664	.624209	.919452	.321106	.271462
1.54	.367661	.622429	.918361	.322239	.271772
1.55	.368668	.620634	.917261	.323384	.272085
1.56	.369686	.618823	.916153	.324542	.272400
1.57	.370714	.616996	.915037	.325714	.272718
1.58	.371752	.615154	.913913	.326901	.273040
1.59	.372801	.613296	.912781	.328101	.273364
1.60	.373861	.611423	.911641	.329316	.273691
1.61	.374931	.609533	.910492	.330546	.274021
1.62	.376012	.607627	.909335	.331790	.274354
1.63	.377104	.605703	.908170	.333049	.274690
1.64	.378207	.603766	.906997	.334323	.275029
1.65	.379321	.601812	.905815	.335613	.275371
1.66	.380446	.599840	.904625	.336918	.275716
1.67	.381583	.597853	.903427	.338239	.276064
1.68	.382731	.595848	.902220	.339576	.276415
1.69	.383891	.593826	.901005	.340929	.276769
1.70	.385062	.591788	.899781	.342298	.277126
1.71	.386245	.589732	.898549	.343684	.277487
1.72	.387440	.587660	.897308	.345086	.277851
1.73	.388648	.585570	.896060	.346506	.278218
1.74	.389867	.583462	.894802	.347943	.278588
1.75	.391098	.581337	.893536	.349397	.278961
1.76	.392342	.579194	.892261	.350869	.279338
1.77	.393598	.577034	.890978	.352359	.279717
1.78	.394868	.574855	.889686	.353867	.280101
1.79	.396149	.572659	.888386	.355394	.280487
1.80	.397444	.570444	.887077	.356939	.280877
1.81	.398752	.568211	.885759	.358504	.281271
1.82	.400073	.565960	.884432	.360087	.281667
1.83	.401407	.563689	.883097	.361690	.282068
1.84	.402754	.561401	.881753	.363313	.282471
1.85	.404116	.559093	.880400	.364956	.282878
1.86	.405491	.556766	.879038	.366619	.283289
1.87	.406879	.554420	.877667	.368302	.283703
1.88	.408282	.552055	.876288	.370007	.284121
1.89	.409699	.549670	.874899	.371733	.284543

TABLE I (Continued)
COMPRESSION

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S^2}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
1.90	0.611131	0.547266	0.873502	0.373460	0.254965
1.91	.612576	.544842	.872095	.375250	.255396
1.92	.614037	.542395	.870680	.377041	.255829
1.93	.615512	.539933	.869255	.378835	.256265
1.94	.617002	.537449	.867822	.380692	.256705
1.95	.618508	.534944	.866379	.382552	.257148
1.96	.620025	.532419	.864927	.384435	.257596
1.97	.621565	.529872	.863466	.386343	.258047
1.98	.623117	.527305	.861996	.388274	.258502
1.99	.624684	.524717	.860517	.390230	.258961
2.00	.626268	.522107	.859028	.392211	.259424
2.01	.627868	.519476	.857530	.394218	.259891
2.02	.629484	.516823	.856023	.396250	.260362
2.03	.631117	.514149	.854506	.398309	.260837
2.04	.632767	.511452	.852980	.400393	.261316
2.05	.634433	.508733	.851444	.402505	.261799
2.06	.636117	.505992	.849899	.404645	.262286
2.07	.637818	.503228	.848345	.406812	.262778
2.08	.639537	.500441	.846781	.409007	.263274
2.09	.641273	.497631	.845207	.411231	.263773
2.10	.643028	.494798	.843624	.413485	.264278
2.11	.644800	.491942	.842031	.415768	.264786
2.12	.646592	.489062	.840429	.418081	.265299
2.13	.648401	.486157	.838816	.420424	.265816
2.14	.650230	.483229	.837194	.422799	.266338
2.15	.652078	.480276	.835562	.425206	.266864
2.16	.653945	.477299	.833921	.427644	.267394
2.17	.655832	.474297	.832269	.430116	.267929
2.18	.657739	.471270	.830608	.432620	.268469
2.19	.659666	.468217	.828937	.435159	.269013
2.20	.661613	.465139	.827256	.437732	.269562
2.21	.663581	.462036	.825564	.440339	.270116
2.22	.665570	.458906	.823862	.442983	.270674
2.23	.667579	.455749	.822151	.445662	.271237
2.24	.669611	.452566	.820429	.448378	.271805
2.25	.671664	.449357	.818697	.451132	.272378
2.26	.673739	.446120	.816955	.453924	.272956
2.27	.675836	.442855	.815203	.456754	.273539
2.28	.677956	.439563	.813440	.459624	.274127
2.29	.680099	.436243	.811667	.462534	.274719
2.30	.682265	.432898	.809884	.465485	.275317
2.31	.684454	.429518	.808090	.468478	.275920
2.32	.686668	.426112	.806286	.471512	.276529
2.33	.688905	.422677	.804471	.474590	.277142
2.34	.691167	.419212	.802645	.477712	.277761
2.35	.693454	.415718	.800809	.480878	.278385
2.36	.695766	.412193	.798963	.484090	.279014
2.37	.698103	.408638	.797105	.487348	.279649
2.38	.700466	.405051	.795237	.490653	.280290
2.39	.702856	.401434	.793358	.494006	.280936
2.40	.705272	.397785	.791468	.497409	.281587

TABLE I (Continued)
COMPRESSION

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
2.41	.707715	.394104	.789567	.500861	.312245
2.42	.710186	.390891	.787655	.504363	.312908
2.43	.712654	.386645	.785733	.507918	.313576
2.44	.715210	.382866	.783799	.511525	.314251
2.45	.717765	.379053	.781854	.515186	.314931
2.46	.720349	.375207	.779898	.518902	.315617
2.47	.722962	.371326	.777930	.522674	.316310
2.48	.725605	.367411	.775952	.526503	.317008
2.49	.728279	.363461	.773962	.530390	.317713
2.50	.730983	.359475	.771961	.534336	.318423
2.51	.733718	.355453	.769948	.538342	.319140
2.52	.736485	.351394	.767924	.542410	.319863
2.53	.739284	.347299	.765888	.546541	.320593
2.54	.742116	.343167	.763841	.550736	.321328
2.55	.744980	.338996	.761782	.554996	.322071
2.56	.747879	.334788	.759712	.559323	.322820
2.57	.750812	.330540	.757629	.563718	.323576
2.58	.753779	.326253	.755535	.568183	.324338
2.59	.756781	.321927	.753429	.572718	.325107
2.60	.759820	.317560	.751311	.577326	.325882
2.61	.762894	.313152	.749181	.582008	.326665
2.62	.766006	.308703	.747040	.586765	.327455
2.63	.769155	.304211	.744885	.591600	.328252
2.64	.772342	.299678	.742719	.596513	.329055
2.65	.775568	.295101	.740541	.601506	.329866
2.66	.778834	.290480	.738350	.606582	.330685
2.67	.782139	.285815	.736147	.611742	.331510
2.68	.785485	.281105	.733931	.616987	.332343
2.69	.788873	.276349	.731703	.622320	.333184
2.70	.792302	.271547	.729462	.627743	.334032
2.71	.795775	.266699	.727209	.633257	.334888
2.72	.799290	.261802	.724943	.638865	.335751
2.73	.802850	.256858	.722665	.644569	.336622
2.74	.806455	.251864	.720373	.650370	.337501
2.75	.810106	.246820	.718069	.656272	.338389
2.76	.813803	.241727	.715751	.662276	.339284
2.77	.817548	.236581	.713421	.668385	.340187
2.78	.821341	.231384	.711078	.674600	.341099
2.79	.825182	.226134	.708721	.680926	.342019
2.80	.829074	.220831	.706351	.687364	.342947
2.81	.833017	.215473	.703968	.693917	.343883
2.82	.837011	.210060	.701571	.700587	.344820
2.83	.841057	.204590	.699161	.707378	.345765
2.84	.845158	.199064	.696737	.714292	.346718
2.85	.849313	.193479	.694300	.721332	.347678
2.86	.853523	.187836	.691849	.728502	.348640
2.87	.857790	.182133	.689384	.735804	.349609
2.88	.862115	.176369	.686906	.743242	.350691
2.89	.866498	.170543	.684413	.750819	.351699

TABLE I (continued)

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S^2}{EI}$	$\frac{S}{EI}$	C^2	$\frac{S^2 C^2}{EI^2}$
2.90	.0370941	.0164654	.0681906	.0758539	.0352718
2.91	.0754446	.158701	.679386	.766408	.353746
2.92	.080012	.152683	.676850	.774421	.354783
2.93	.084442	.146599	.674301	.782591	.355830
2.94	.089336	.140448	.671738	.790919	.356888
2.95	.094096	.134228	.669160	.799408	.357955
2.96	.098923	.127959	.666567	.808063	.359032
2.97	.103819	.121579	.663960	.816888	.360119
2.98	.108784	.115147	.661338	.825889	.361216
2.99	.113821	.108641	.658702	.835068	.362326
3.00	.118930	.102060	.656050	.844432	.363444
3.01	.124113	.0954039	.653384	.853988	.364575
3.02	.129372	.0886698	.650701	.863738	.365715
3.03	.134708	.0818568	.648005	.873679	.366866
3.04	.140123	.0749633	.645292	.883800	.368028
3.05	.145618	.0679879	.642565	.894193	.369203
3.06	.151195	.0609290	.639822	.904772	.370389
3.07	.156856	.0537850	.637063	.915573	.371585
3.08	.162603	.0465543	.634289	.926604	.372793
3.09	.168437	.0392350	.631499	.937870	.374014
3.10	.174360	.0318257	.628694	.949376	.375248
3.11	.180375	.0243243	.625872	.961135	.376491
3.12	.186488	.0167291	.623035	.973149	.377749
3.13	.192687	.00903818	.620182	.985427	.379021
3.14	.198987	.00124960	.617242	.997976	.380316
π	1.00000	0	.616850	1.00000	.380504
3.15	1.00539	-.00663866	.614429	1.01080	.381602
3.16	1.01189	-.0146287	.611520	1.02392	.382703
3.17	1.01850	-.0227226	.608598	1.03734	.383821
3.18	1.02521	-.0309225	.605663	1.05106	.384956
3.19	1.03203	-.0392308	.602708	1.06509	.386102
3.20	1.03897	-.0476498	.599738	1.07945	.387263
3.21	1.04601	-.0561818	.596750	1.09416	.388437
3.22	1.05318	-.0648294	.593745	1.10919	.389626
3.23	1.06046	-.0735951	.590723	1.12458	.390828
3.24	1.06787	-.0824816	.587683	1.14035	.392044
3.25	1.07541	-.0914915	.584625	1.15650	.393275
3.26	1.08307	-.100628	.581551	1.17303	.394521
3.27	1.09086	-.109893	.578459	1.18998	.395783
3.28	1.09879	-.119290	.575348	1.20734	.397058
3.29	1.10686	-.128823	.572218	1.22513	.401149
3.30	1.11506	-.138494	.569072	1.24337	.402256
3.31	1.12342	-.148307	.565906	1.26207	.404178
3.32	1.13192	-.158266	.562723	1.28125	.405716
3.33	1.14058	-.168372	.559520	1.30092	.407270
3.34	1.14939	-.178632	.556299	1.32111	.408841
3.35	1.15837	-.189047	.553058	1.34182	.410427
3.36	1.16751	-.199622	.549799	1.36308	.412031
3.37	1.17682	-.210362	.546521	1.38491	.413652
3.38	1.18631	-.221270	.543223	1.40733	.415290
3.39	1.19597	-.232350	.539905	1.43035	.416945
3.40	1.20582	-.243607	.536569	1.45401	.418618

TABLE I (continued)

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
3.41	1.21586	-.255047	.533212	1.47832	.420309
3.42	1.22610	-.266673	.529836	1.50331	.422018
3.43	1.23653	-.278491	.526438	1.52901	.423746
3.44	1.24717	-.290505	.523021	1.55544	.425492
3.45	1.25802	-.302722	.519584	1.58262	.427257
3.46	1.26909	-.315147	.516126	1.61060	.429041
3.47	1.28039	-.327785	.512648	1.63940	.430846
3.48	1.29192	-.340644	.509148	1.66905	.432670
3.49	1.30368	-.353728	.505627	1.69958	.434514
3.50	1.31569	-.367045	.502085	1.73104	.436378
3.51	1.32795	-.380602	.498522	1.76346	.438262
3.52	1.34048	-.394405	.494937	1.79688	.440168
3.53	1.35327	-.408463	.491330	1.83134	.442095
3.54	1.36634	-.422782	.487701	1.86689	.444044
3.55	1.37970	-.437371	.484051	1.90356	.446014
3.56	1.39335	-.452238	.480377	1.94142	.448007
3.57	1.40731	-.467392	.476682	1.98051	.450022
3.58	1.42158	-.482841	.472963	2.02089	.452061
3.59	1.43618	-.498597	.469222	2.06260	.454122
3.60	1.45111	-.514668	.465457	2.10572	.456207
3.61	1.46639	-.531064	.461670	2.15031	.458315
3.62	1.48204	-.547798	.457859	2.19643	.460448
3.63	1.49805	-.564879	.454024	2.24416	.462606
3.64	1.51445	-.582321	.450165	2.29357	.464789
3.65	1.53126	-.600135	.446282	2.34474	.466997
3.66	1.54847	-.618335	.442375	2.39776	.469231
3.67	1.56612	-.636934	.438443	2.45272	.471491
3.68	1.58420	-.655946	.434486	2.50971	.473778
3.69	1.60276	-.675387	.430505	2.56883	.476091
3.70	1.62179	-.695273	.426498	2.63019	.478432
3.71	1.64131	-.715619	.422465	2.69391	.480801
3.72	1.66136	-.736445	.418407	2.76011	.483199
3.73	1.68194	-.757776	.414323	2.82895	.485628
3.74	1.70308	-.779606	.410213	2.90049	.488080
3.75	1.72480	-.801982	.406077	2.97495	.490565
3.76	1.74718	-.824916	.401914	3.05247	.493080
3.77	1.77009	-.848432	.397723	3.13322	.495625
3.78	1.79371	-.872553	.393506	3.21738	.498202
3.79	1.81801	-.897304	.389261	3.30514	.500810
3.80	1.84302	-.922712	.384989	3.39672	.503451
3.81	1.86878	-.948807	.380689	3.49234	.506124
3.82	1.89532	-.975617	.376360	3.59224	.508830
3.83	1.92268	-.100318	.372003	3.69669	.511570
3.84	1.95088	-.103151	.367617	3.80695	.514343
3.85	1.97998	-.106067	.363202	3.92234	.517154
3.86	2.01002	-.109069	.358758	4.04401	.519999
3.87	2.04103	-.112159	.354284	4.16581	.522879
3.88	2.07307	-.115344	.349780	4.29763	.525797

TABLE I (continued)

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
3.89	2.10619	-1.18628	0.345245	4.43605	0.528752
3.90	2.14045	-1.22015	.340680	4.58151	.531744
3.91	2.17589	-1.25511	.336085	4.73450	.534775
3.92	2.21259	-1.29121	.331458	4.89555	.537846
3.93	2.25061	-1.32852	.326799	5.06524	.540956
3.94	2.29002	-1.36709	.322109	5.24419	.544107
3.95	2.33090	-1.40701	.317386	5.43311	.547299
3.96	2.37334	-1.44834	.312631	5.63273	.550533
3.97	2.41741	-1.49116	.307848	5.84388	.553810
3.98	2.46323	-1.53556	.303022	6.06748	.557130
3.99	2.51088	-1.58163	.298167	6.30452	.560495
4.00	2.56049	-1.62948	.293279	6.55610	.563905
4.01	2.61217	-1.67922	.288355	6.82343	.567361
4.02	2.66606	-1.73096	.283398	7.10787	.570863
4.03	2.72230	-1.78482	.278405	7.41090	.574413
4.04	2.78104	-1.84097	.273376	7.73418	.578011
4.05	2.84246	-1.89953	.268312	8.07955	.581659
4.06	2.90679	-1.96069	.263212	8.44909	.585356
4.07	2.97407	-2.02462	.258076	8.84310	.589105
4.08	3.04469	-2.09153	.252900	9.27016	.592906
4.09	3.11885	-2.16163	.247689	9.72720	.596760
4.10	3.19680	-2.23517	.242439	10.2195	.600668
4.11	3.27885	-2.31241	.237151	10.7508	.604631
4.12	3.36532	-2.39366	.231824	11.3254	.608650
4.13	3.45656	-2.47924	.226457	11.9479	.612726
4.14	3.55304	-2.56952	.221051	12.6241	.616861
4.15	3.65515	-2.66491	.215605	13.3602	.621054
4.16	3.76343	-2.76587	.210118	14.1634	.625308
4.17	3.87843	-2.87290	.204590	15.0422	.629624
4.18	4.00082	-2.98660	.199020	16.0065	.634003
4.19	4.13130	-3.10762	.193408	17.0677	.638445
4.20	4.27073	-3.23670	.187753	18.2391	.642953
4.21	4.42004	-3.37471	.182055	19.5367	.647527
4.22	4.58031	-3.52261	.176313	20.9793	.652170
4.23	4.75280	-3.68159	.170527	22.5891	.656881
4.24	4.93895	-3.85278	.164696	24.3833	.661663
4.25	5.14045	-4.03787	.158820	26.3743	.666517
4.26	5.35927	-4.23858	.152897	28.5721	.671445
4.27	5.59774	-4.45701	.146928	31.0347	.676448
4.28	5.85861	-4.69564	.140912	34.8323	.681527
4.29	6.14320	-4.95746	.134847	37.7634	.686684
4.30	6.46148	-5.24604	.128735	41.7508	.691921
4.31	6.81233	-5.56579	.122573	46.9079	.697240
4.32	7.20372	-5.92207	.116362	51.8937	.702641
4.33	7.64310	-6.32159	.110100	56.4170	.708127
4.34	8.13984	-6.77281	.103787	66.2370	.713780
4.35	8.70395	-7.28634	.0974220	75.7956	.719561
4.36	9.35704	-7.87684	.0910048	87.5541	.725412
4.37	10.1137	-8.56231	.0845344	102.238	.730955
4.38	11.0040	-9.36812	.0780101	121.089	.736893
4.39	12.0666	-10.3292	.0714311	145.603	.742927
4.40	13.3569	-11.4953	.0647967	178.406	.749059

TABLE I (continued)

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
4.41	14.9567	-12.9404	.0581061	223.703	.755292
4.42	16.9926	-14.7783	.0513585	288.747	.761627
4.43	19.6708	-17.1948	.0445531	386.739	.768067
4.44	23.3522	-20.5151	.0376891	545.324	.774615
4.45	28.7300	-25.3636	.0307656	825.413	.781272
4.46	37.3277	-33.1126	.0237817	1293.35	.788041
4.47	53.2714	-47.4793	.0167367	2337.84	.794925
4.48	92.9960	-83.2686	.00962948	8648.26	.801926
4.49	365.751	-328.980	.00245924	133774	.809047
4.50	189.813 168.680	170.445 147	7493 -.00478848	35801.6 35600.0	.816291
4.51	-75.1653	68.2048	-.0120741	5644.83	.823668
4.52	-46.8989	42.7873	-.0194392	2199.51	.831138
4.53	-34.0830	31.1882	-.0268713	1161.65	.838787
4.54	-26.7689	24.3953	-.0343712	716.677	.846551
4.55	-22.0401	20.3312	-.0419402	485.765	.854452
4.56	-18.7317	17.3467	-.0495793	350.878	.862495
4.57	-16.2875	15.1406	-.0572895	265.283	.870682
4.58	-14.4080	13.4433	-.0650721	207.590	.879016
4.59	-12.9178	12.0966	-.0729281	166.871	.887502
4.60	-11.7074	11.0020	-.0808387	137.864	.896148
4.61	-10.7048	10.0946	-.0888681	114.593	.904943
4.62	-9.86073	9.32975	-.0969487	97.2340	.913906
4.63	-9.14036	8.67647	-.105110	83.5462	.923036
4.64	-8.51839	8.11180	-.113352	72.5638	.932337
4.65	-7.97597	7.61877	-.121674	63.6161	.941813
4.66	-7.49578	7.18447	-.130079	56.2316	.951469
4.67	-7.07572	6.79892	-.138567	50.0639	.961309
4.68	-6.69811	6.45429	-.147141	44.8647	.971338
4.69	-6.35901	6.14431	-.155801	40.4370	.981561
4.70	-6.05282	5.86397	-.164549	36.6367	.991984
4.71	-5.77499	5.60914	-.173386	33.3506	1.00261
4.72	-5.52177	5.37645	-.182315	30.4899	1.01345
4.73	-5.29003	5.16209	-.191336	27.9844	1.02450
4.74	-5.07716	4.96671	-.200452	25.7775	1.03577
4.75	-4.88096	4.78531	-.209664	23.8237	1.04727
4.76	-4.69954	4.61722	-.218974	22.0857	1.05900
4.77	-4.53132	4.46097	-.228383	20.5329	1.07097
4.78	-4.37490	4.31534	-.237894	19.1398	1.08318
4.79	-4.22910	4.17924	-.247507	17.8853	1.09565
4.80	-4.09288	4.05174	-.257227	16.7516	1.10838
4.81	-3.96532	3.93202	-.267058	15.7237	1.12137
4.82	-3.84563	3.81937	-.276988	14.7889	1.13464
4.83	-3.73312	3.71315	-.287035	13.9362	1.14819
4.84	-3.62716	3.61280	-.297196	13.1563	1.16203
4.85	-3.52721	3.51784	-.307471	12.4412	1.17617
4.86	-3.43276	3.42781	-.317865	11.7837	1.19062
4.87	-3.34339	3.34232	-.328379	11.1782	1.20538
4.88	-3.25869	3.26102	-.339015	10.6191	1.22047

TABLE I (continued)

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
4.89	-3.17835	3.18358	-0.349777	10.1018	1.23589
4.90	-3.10197	3.10973	-.360666	9.62219	1.25165
4.91	-3.02932	3.03919	-.371685	9.17680	1.26777
4.92	-2.96014	2.97175	-.382837	8.76244	1.28426
4.93	-2.89418	2.90717	-.394124	8.37628	1.30112
4.94	-2.83122	2.84527	-.405550	8.01583	1.31837
4.95	-2.77108	2.78587	-.417117	7.67886	1.33602
4.96	-2.71356	2.72880	-.428829	7.36339	1.35408
4.97	-2.65850	2.67393	-.440687	7.06763	1.37257
4.98	-2.60576	2.62110	-.452697	6.78997	1.39150
4.99	-2.55519	2.57020	-.464860	6.52878	1.41088
5.00	-2.50666	2.52111	-.477180	6.28335	1.43073
5.01	-2.46006	2.47373	-.489661	6.05191	1.45106
5.02	-2.41528	2.42794	-.502307	5.83358	1.47188
5.03	-2.37222	2.38367	-.515120	5.62741	1.49323
5.04	-2.33077	2.34083	-.528106	5.43281	1.51510
5.05	-2.29087	2.29924	-.541267	5.24807	1.53752
5.06	-2.25241	2.25912	-.554607	5.07337	1.56052
5.07	-2.21534	2.22011	-.568132	4.90774	1.58409
5.08	-2.17958	2.18225	-.581845	4.75037	1.60828
5.09	-2.14506	2.14547	-.595752	4.60129	1.63309
5.10	-2.11173	2.10973	-.609855	4.45939	1.65855
5.11	-2.07952	2.07496	-.624161	4.32440	1.68469
5.12	-2.04833	2.04112	-.638675	4.19587	1.71152
5.13	-2.01827	2.00517	-.653400	4.07341	1.73907
5.14	-1.98913	1.97606	-.668344	3.95665	1.76737
5.15	-1.96093	1.94475	-.683511	3.84523	1.79644
5.16	-1.93361	1.91420	-.698906	3.73883	1.82632
5.17	-1.90715	1.88438	-.714536	3.63721	1.85702
5.18	-1.88150	1.85526	-.730408	3.54004	1.88859
5.19	-1.85663	1.82681	-.746526	3.44707	1.92106
5.20	-1.83251	1.79898	-.762898	3.35809	1.95446
5.21	-1.80910	1.77176	-.779531	3.27286	1.98881
5.22	-1.78639	1.74513	-.796432	3.19118	2.02416
5.23	-1.76433	1.71904	-.813607	3.11286	2.06058
5.24	-1.74291	1.69349	-.831065	3.03773	2.09807
5.25	-1.72210	1.66844	-.848813	2.96561	2.13668
5.26	-1.70187	1.64388	-.866860	2.89636	2.17646
5.27	-1.68221	1.61978	-.885214	2.82982	2.21746
5.28	-1.66309	1.59614	-.903884	2.76586	2.25973
5.29	-1.64449	1.57292	-.922879	2.70436	2.30332
5.30	-1.62640	1.55011	-.942210	2.64518	2.34828
5.31	-1.60880	1.52769	-.961884	2.58823	2.39468
5.32	-1.59166	1.50565	-.981914	2.53348	2.44258
5.33	-1.57498	1.48398	-.100231	2.48086	2.49203
5.34	-1.55873	1.46266	-.102305	2.42965	2.54311
5.35	-1.54291	1.44166	-.104424	2.38057	2.59589
5.36	-1.52750	1.42098	-.106581	2.33325	2.65044
5.37	-1.51248	1.40062	-.108778	2.28769	2.70685
5.38	-1.49784	1.38055	-.111019	2.24338	2.76519
5.39	-1.48358	1.36077	-.113303	2.20100	2.82557
5.40	-1.46967	1.34126	-.115634	2.15993	2.88807

TABLE I (continued)

$\left(\frac{L}{j}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
5.41	-1.45611	1.32202	-1.18011	2.12025	2.95278
5.42	-1.44289	1.30303	-1.20437	2.08192	3.01963
5.43	-1.42999	1.28428	-1.22913	2.04487	3.08931
5.44	-1.41741	1.26577	-1.25442	2.00905	3.16136
5.45	-1.40514	1.24748	-1.28024	1.97441	3.23609
5.46	-1.39316	1.22940	-1.30662	1.94090	3.31363
5.47	-1.38148	1.21154	-1.33358	1.90848	3.39414
5.48	-1.37008	1.19387	-1.36115	1.87711	3.47775
5.49	-1.35895	1.17640	-1.38933	1.84674	3.56468
5.50	-1.34809	1.15911	-1.41816	1.81733	3.65496
5.51	-1.33748	1.14200	-1.44766	1.78886	3.74894
5.52	-1.32713	1.12506	-1.47785	1.76128	3.84678
5.53	-1.31703	1.10828	-1.50877	1.73456	3.94854
5.54	-1.30716	1.09166	-1.54044	1.70867	4.05441
5.55	-1.29753	1.07519	-1.57289	1.68358	4.16516
5.56	-1.28812	1.05887	-1.60616	1.65926	4.28047
5.57	-1.27894	1.04269	-1.64027	1.63566	4.40079
5.58	-1.26997	1.02664	-1.67527	1.61282	4.52641
5.59	-1.26121	1.01071	-1.71119	1.59065	4.65767
5.60	-1.25266	.994913	-1.74806	1.56915	4.79489
5.61	-1.24431	.979230	-1.78594	1.54830	4.93843
5.62	-1.23615	.963660	-1.82487	1.52807	5.08870
5.63	-1.22819	.948198	-1.86489	1.50848	5.24609
5.64	-1.22041	.932838	-1.90605	1.48941	5.41108
5.65	-1.21282	.917577	-1.94842	1.47093	5.58416
5.66	-1.20541	.902410	-1.99204	1.45301	5.76585
5.67	-1.19817	.887333	-2.03697	1.43561	5.95674
5.68	-1.19111	.872339	-2.08329	1.41873	6.15744
5.69	-1.18421	.857427	-2.13106	1.40235	6.36864
5.70	-1.17748	.842593	-2.18036	1.38648	6.59107
5.71	-1.17090	.827831	-2.23124	1.37102	6.82554
5.72	-1.16449	.813139	-2.28382	1.35604	7.07290
5.73	-1.15824	.798512	-2.33818	1.34151	7.33415
5.74	-1.15213	.783947	-2.39441	1.32741	7.61031
5.75	-1.14618	.769440	-2.45263	1.31372	7.90253
5.76	-1.14037	.754987	-2.51293	1.30044	8.21206
5.77	-1.13471	.740586	-2.57545	1.28756	8.54029
5.78	-1.12918	.726233	-2.64031	1.27506	8.88875
5.79	-1.12380	.711924	-2.70766	1.26293	9.25909
5.80	-1.11856	.697656	-2.77765	1.25117	9.65219
5.81	-1.11345	.683427	-2.85045	1.23976	10.0731
5.82	-1.10847	.669232	-2.92623	1.22870	10.5211
5.83	-1.10362	.655069	-3.00519	1.21798	10.9998
5.84	-1.09890	.640934	-3.08758	1.20759	11.5119
5.85	-1.09431	.626825	-3.17354	1.19752	12.0606
5.86	-1.08984	.612787	-3.26342	1.18776	12.6493
5.87	-1.08550	.598862	-3.35747	1.17831	13.2822
5.88	-1.08128	.584963	-3.45599	1.16916	13.9644

TABLE I (concluded)

$\left(\frac{L}{J}\right)_{eff}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
5.89	-1.07710	0.570587	-3.55933	1.16031	14.6998
5.90	-1.07319	.556562	-3.66787	1.16174	15.4946
5.91	-1.06932	.542546	-3.78201	1.16345	16.3555
5.92	-1.06557	.528535	-3.90222	1.16544	17.2898
5.93	-1.06193	.514527	-4.02902	1.16771	18.3061
5.94	-1.05841	.500518	-4.16298	1.17023	19.4140
5.95	-1.05500	.486507	-4.30474	1.17302	20.6250
5.96	-1.05169	.472491	-4.45502	1.17606	21.9521
5.97	-1.04850	.458466	-4.61463	1.09935	23.4105
5.98	-1.04541	.444431	-4.78450	1.09289	25.0178
5.99	-1.04244	.430382	-4.96569	1.08667	26.7953
6.00	-1.03956	.416317	-5.15938	1.08069	28.7471
6.01	-1.03680	.402234	-5.36694	1.07495	30.8762
6.02	-1.03413	.388129	-5.58995	1.06943	33.1711
6.03	-1.03158	.373999	-5.83026	1.06415	35.6324
6.04	-1.02912	.359843	-6.08996	1.05909	38.2790
6.05	-1.02677	.345658	-6.37157	1.05423	42.1993
6.06	-1.02452	.331441	-6.67502	1.04963	46.5098
6.07	-1.02236	.317189	-7.01282	1.04523	51.4041
6.08	-1.02031	.302899	-7.38803	1.04104	56.9018
6.09	-1.01837	.288570	-7.78502	1.03707	62.5531
6.10	-1.01651	.274197	-8.23357	1.03330	70.0494
6.11	-1.01476	.259780	-8.73351	1.02975	78.5430
6.12	-1.01311	.245314	-9.29412	1.02639	88.6607
6.13	-1.01156	.230797	-9.92736	1.02325	100.844
6.14	-1.01010	.216227	-10.6483	1.02031	115.688
6.15	-1.00874	.201600	-11.4768	1.01757	134.031
6.16	-1.00749	.186914	-12.4392	1.01503	157.058
6.17	-1.00632	.172166	-13.5707	1.01269	186.501
6.18	-1.00526	.157353	-14.9205	1.01055	224.970
6.19	-1.00429	.142472	-16.5591	1.00860	276.565
6.20	-1.00342	.127521	-18.5908	1.00686	347.990
6.21	-1.00265	.112495	-21.1758	1.00531	450.798
6.22	-1.00198	.0973934	-24.5774	1.00396	606.443
6.23	-1.00140	.0822118	-29.2572	1.00281	858.388
6.24	-1.00093	.0669474	-36.1085	1.00185	1206.24
6.25	-1.00055	.0515970	-47.0647	1.00110	2217.51
6.26	-1.00027	.0361576	-67.4745	1.00054	4555.25
6.27	-1.00009	.0206258	-118.806	1.00017	14117.2
6.28	-1.00001	.00499841	-490.041	1.00001	240142
2π	-1.00000	0	-∞	1.00000	∞

TABLE II
TENSION

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
0	0.500000	0.750000	1.00000	0.250000	0.250000
.1	.499757	.750512	1.00036	.249757	.249756
.2	.499001	.751998	1.00133	.249002	.249665
.3	.497760	.754488	1.00300	.247765	.249253
.4	.496033	.757964	1.00532	.246049	.248675
.5	.493831	.762412	1.00831	.243869	.247937
.6	.491167	.767818	1.01194	.241245	.247042
.7	.488057	.774165	1.01623	.238200	.245994
.8	.484519	.781431	1.02116	.234759	.244798
.9	.480575	.789595	1.02672	.230953	.243469
1.0	.476246	.798632	1.03291	.226810	.241983
1.1	.471556	.808615	1.03971	.222365	.240376
1.2	.466530	.819216	1.04712	.217651	.238646
1.3	.461194	.830703	1.05513	.212700	.236799
1.4	.455575	.842949	1.06372	.207548	.234843
1.5	.449699	.855921	1.07289	.202229	.232785
1.6	.443594	.869556	1.08262	.196775	.230633
1.7	.437286	.883915	1.09290	.191219	.228396
1.8	.430802	.898873	1.10371	.185590	.226081
1.9	.424167	.914429	1.11505	.179918	.223697
2.0	.417408	.930653	1.12689	.174229	.221251
2.1	.410548	.947214	1.13923	.168550	.218751
2.2	.403610	.964380	1.15205	.162901	.216205
2.3	.396616	.982024	1.16534	.157305	.213621
2.4	.389588	1.00012	1.17908	.151779	.211006
2.5	.382544	1.01863	1.19325	.146340	.208366
2.6	.375502	1.03754	1.20785	.141002	.205709
2.7	.368480	1.05683	1.22287	.135777	.203042
2.8	.361492	1.07646	1.23827	.130677	.200369
2.9	.354553	1.09642	1.25406	.125708	.197697
3.0	.347676	1.11665	1.27022	.120878	.195032
3.1	.340871	1.13722	1.28673	.116193	.192378
3.2	.334149	1.15803	1.30358	.111656	.189740
3.3	.327520	1.17909	1.32076	.107269	.187122
3.4	.320990	1.20037	1.33826	.103034	.184529
3.5	.314566	1.22188	1.35606	.0989519	.181963
3.6	.308253	1.24358	1.37416	.0950214	.179429
3.7	.302062	1.26547	1.39253	.0912413	.176929
3.8	.295990	1.28754	1.41117	.0876098	.174466
3.9	.290042	1.30976	1.43007	.0841242	.172042
4.0	.284221	1.33214	1.44921	.0807815	.169658
4.1	.278529	1.35466	1.46859	.0775783	.167318
4.2	.272967	1.37731	1.48820	.0745108	.165022
4.3	.267535	1.40009	1.50802	.0715749	.162771
4.4	.262234	1.42297	1.52805	.0687666	.160566
4.5	.257063	1.44597	1.54828	.0660813	.158409
4.6	.252022	1.46907	1.56870	.0635181	.156300
4.7	.247110	1.49225	1.58930	.0610631	.154238
4.8	.242324	1.51553	1.61008	.0587210	.152225
4.9	.237664	1.53889	1.63101	.0564843	.150260
5.0	.233128	1.56232	1.65211	.0543486	.148343

TABLE II (continued)

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
5.1	.228713	1.58583	1.67936	.0522097	.146435
5.2	.224418	1.60940	1.69476	.0503634	.144654
5.3	.220239	1.63304	1.71629	.0485064	.142880
5.4	.216176	1.65674	1.73793	.0467319	.141153
5.5	.212224	1.68049	1.75974	.0450388	.139472
5.6	.208381	1.70429	1.78166	.0434225	.137836
5.7	.204645	1.72814	1.80368	.0418794	.136246
5.8	.201012	1.75204	1.82582	.0404059	.134698
5.9	.197481	1.77599	1.84806	.0389787	.133193
6.0	.194048	1.79997	1.87040	.0376547	.131731
6.1	.190711	1.82400	1.89284	.0363706	.130310
6.2	.187466	1.84806	1.91537	.0351427	.128930
6.3	.184312	1.87215	1.93799	.0339710	.127588
6.4	.181245	1.89628	1.96069	.0328499	.126285
6.5	.178264	1.92044	1.98348	.0317799	.125020
6.6	.175364	1.94463	2.00633	.0307526	.123777
6.7	.172544	1.96885	2.02927	.0297715	.122597
6.8	.169802	1.99310	2.05227	.0288326	.121438
6.9	.167134	2.01737	2.07534	.0279338	.120312
7.0	.164539	2.04166	2.09847	.0270730	.119218
7.1	.162013	2.06598	2.12167	.0262484	.118157
7.2	.159556	2.09032	2.14493	.0254582	.117125
7.3	.157164	2.11468	2.16824	.0247007	.116124
7.4	.154836	2.13906	2.19160	.0239743	.115151
7.5	.152570	2.16346	2.21502	.0232775	.114207
7.6	.150363	2.18788	2.23849	.0226089	.113289
7.7	.148213	2.21231	2.26200	.0219671	.112398
7.8	.146119	2.23676	2.28556	.0213507	.111532
7.9	.144079	2.26123	2.30917	.0207586	.110690
8.0	.142090	2.28571	2.33281	.0201897	.109872
8.1	.140152	2.31021	2.35650	.0196427	.109078
8.2	.138263	2.33472	2.38022	.0191167	.108305
8.3	.136421	2.35925	2.40399	.0186107	.107554
8.4	.134625	2.38378	2.42778	.0181238	.106824
8.5	.132872	2.40833	2.45162	.0176550	.106114
8.6	.131162	2.43289	2.47548	.0172035	.105428
8.7	.129494	2.45747	2.49938	.0167686	.104752
8.8	.127865	2.48208	2.52331	.0163495	.104098
8.9	.126275	2.50665	2.54726	.0159454	.103462
9.0	.124722	2.53125	2.57125	.0155557	.102843
9.1	.123206	2.55586	2.59526	.0151797	.102241
9.2	.121724	2.58049	2.61930	.0148169	.101654
9.3	.120277	2.60512	2.64336	.0144666	.101083
9.4	.118862	2.62976	2.66745	.0141283	.100527
9.5	.117480	2.65441	2.69156	.0138015	.0999848
9.6	.116133	2.67907	2.71569	.0134857	.0994567
9.7	.114806	2.70374	2.73985	.0131804	.0989421
9.8	.113513	2.72841	2.76402	.0128852	.0984405
9.9	.112248	2.75309	2.78822	.0125996	.0979515

TABLE II (continued)

$\left(\frac{L}{J}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C ²	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
10.0	0.111010	2.77778	2.81244	0.0123253	0.0774746
10.1	.109799	2.80247	2.83667	.0120558	.0770094
10.2	.108613	2.82717	2.86092	.0117968	.0765887
10.3	.107452	2.85188	2.88519	.0115460	.0761139
10.4	.106316	2.87668	2.90948	.0113030	.0756810
10.5	.105202	2.90152	2.93379	.0110675	.0752892
10.6	.104112	2.92604	2.95811	.0108392	.0748475
10.7	.103043	2.95077	2.98244	.0106179	.0744454
10.8	.101996	2.97551	3.00679	.0104032	.0740527
10.9	.100969	3.00025	3.03115	.0101948	.0736697
11.0	.0999633	3.02500	3.05553	.00999265	.0732942
11.1	.0989767	3.04975	3.07992	.00979638	.0729279
11.2	.0980092	3.07451	3.10433	.00960580	.0725698
11.3	.0970608	3.09927	3.12875	.00942069	.0722196
11.4	.0961295	3.12404	3.15318	.00924084	.0718773
11.5	.0952169	3.14881	3.17762	.00906607	.0715424
11.6	.0943196	3.17355	3.20207	.00889618	.0712148
11.7	.0934398	3.19836	3.22654	.00873100	.0708943
11.8	.0925762	3.22315	3.25101	.00857036	.0705806
11.9	.0917283	3.24794	3.27550	.00841408	.0702736
12.0	.0908957	3.27273	3.29999	.00826208	.0699730
12.1	.0900780	3.29752	3.32450	.00811404	.0696787
12.2	.0892748	3.32232	3.34901	.00796998	.0693904
12.3	.0884857	3.34712	3.37354	.00782971	.0691081
12.4	.0877103	3.37193	3.39807	.00769310	.0688314
12.5	.0869484	3.39674	3.42261	.00756008	.0685603
12.6	.0861996	3.42155	3.44717	.00743037	.0682947
12.7	.0854635	3.44637	3.47172	.00730400	.0680342
12.8	.0847398	3.47119	3.49629	.00718083	.0677789
12.9	.0840282	3.49601	3.52087	.00706074	.0675285
13.0	.0833284	3.52083	3.54545	.00694363	.0672830
13.1	.0826402	3.54566	3.57004	.00682940	.0670421
13.2	.0819632	3.57049	3.59464	.00671797	.0668058
13.3	.0812972	3.59533	3.61925	.00660923	.0665739
13.4	.0806419	3.62016	3.64386	.00650311	.0663464
13.5	.0799970	3.64500	3.66848	.00639953	.0661230
13.6	.0793624	3.66984	3.69310	.00629839	.0659038
13.7	.0787377	3.69469	3.71773	.00619963	.0656885
13.8	.0781228	3.71953	3.74237	.00610317	.0654771
13.9	.0775174	3.74438	3.76702	.00600905	.0652694
14.0	.0769213	3.76923	3.79167	.00591688	.0650654
14.1	.0763343	3.79408	3.81632	.00582673	.0648651
14.2	.0757561	3.81894	3.84098	.00573899	.0646681
14.3	.0751866	3.84380	3.86568	.00565303	.0644746
14.4	.0746257	3.86866	3.89032	.00556899	.0642843
14.5	.0740730	3.89352	3.91500	.00548681	.0640975
14.6	.0735284	3.91838	3.93968	.00540643	.0639137
14.7	.0729918	3.94325	3.96437	.00532780	.0637330
14.8	.0724630	3.96812	3.98906	.00525088	.0635553
14.9	.0719417	3.99299	4.01376	.00517561	.0633805
15.0	.0714279	4.01786	4.03846	.00510195	.0632085

TABLE II (continued)

$\left(\frac{L}{j}\right)_{\text{eff}}$	C	$\frac{S''}{\left(\frac{EI}{L}\right)}$	$\frac{S}{\left(\frac{EI}{L}\right)}$	C^2	$\frac{S^2 C^2}{\left(\frac{EI}{L}\right)^2}$
15.1	.0709214	4.04278	4.06317	.00502982	.0530394
15.2	.0704220	4.06761	4.08768	.00498926	.0528789
15.3	.0699296	4.09248	4.11259	.00495016	.0527091
15.4	.0694440	4.11736	4.13731	.00491247	.0525480
15.5	.0689651	4.14224	4.16204	.00487619	.0523873
15.6	.0684920	4.16712	4.18676	.00484126	.0522331
15.7	.0680269	4.19201	4.21150	.00480766	.0520794
15.8	.0675673	4.21689	4.23623	.00477534	.0519260
15.9	.0671135	4.24178	4.26097	.00474427	.0517789
16.0	.0666664	4.26667	4.28571	.00471441	.0516321
16.1	.0662249	4.29156	4.31046	.00468574	.0514874
16.2	.0657893	4.31645	4.33521	.00465823	.0513450
16.3	.0653593	4.34134	4.35996	.00463184	.0512046
16.4	.0649349	4.36623	4.38472	.00460654	.0510664
16.5	.0645160	4.39113	4.40948	.00458231	.0509301
16.6	.0641024	4.41603	4.43425	.00455912	.0507958
16.7	.0636941	4.44092	4.45901	.00453694	.0506634
16.8	.0632910	4.46582	4.48378	.00451575	.0505320
16.9	.0628930	4.49072	4.50856	.00449553	.0504043
17.0	.0624999	4.51562	4.53333	.00447624	.0502775
17.1	.0621117	4.54053	4.55811	.00445787	.0501528
17.2	.0617283	4.56543	4.58289	.00444039	.0500292
17.3	.0613496	4.59034	4.60768	.00442378	.0499077
17.4	.0609756	4.61524	4.63247	.00440802	.0497878
17.5	.0606060	4.64015	4.65726	.00439309	.0496695
17.6	.0602409	4.66506	4.68205	.00437897	.0495528
17.7	.0598802	4.68997	4.70685	.00436564	.0494377
17.8	.0595238	4.71488	4.73165	.00435308	.0493241
17.9	.0591716	4.73979	4.75645	.00434127	.0492121
18.0	.0588235	4.76471	4.78125	.00433020	.0491015
18.1	.0584793	4.78962	4.80606	.00431985	.0489923
18.2	.0581393	4.81453	4.83086	.00431020	.0488846
18.3	.0578034	4.83945	4.85567	.00430124	.0487783
18.4	.0574712	4.86437	4.88049	.00429294	.0486733
18.5	.0571428	4.88929	4.90530	.00428530	.0485697
18.6	.0568182	4.91420	4.93012	.00427830	.0484674
18.7	.0564972	4.93912	4.95494	.00427193	.0483664
18.8	.0561798	4.96405	4.97976	.00426617	.0482667
18.9	.0558659	4.98897	5.00459	.00426100	.0481682
19.0	.0555553	5.01389	5.02941	.00425642	.0480709
19.1	.0552486	5.03881	5.05424	.00425241	.0479748
19.2	.0549450	5.06374	5.07907	.00424896	.0478799
19.3	.0546448	5.08866	5.10390	.00424603	.0477861
19.4	.0543478	5.11359	5.12874	.00424369	.0476935
19.5	.0540540	5.13851	5.15357	.00424184	.0476020
19.6	.0537634	5.16344	5.17841	.00424051	.0475116
19.7	.0534759	5.18837	5.20325	.00423968	.0474223
19.8	.0531915	5.21330	5.22809	.00423933	.0473340
19.9	.0529100	5.23823	5.25293	.00423947	.0472467

TABLE II (concluded)

$(\frac{L}{J})_{eff}$	C	$\frac{S''}{(\frac{EI}{L})}$	$\frac{S}{(\frac{EI}{L})}$	C^2	$\frac{S^2 C^2}{(\frac{EI}{L})^2}$
20	.0526916	5.26916	5.27778	.00277008	.07771608
21	.0500000	5.51250	5.52432	.00250000	.0763504
22	.0476190	5.76190	5.77509	.00226757	.0756258
23	.0454545	6.01136	6.02301	.00206612	.0749716
24	.0434753	6.26087	6.27273	.00189036	.0743502
25	.0416667	6.51042	6.52174	.00173611	.0738422
26	.0400000	6.76000	6.77083	.00160000	.0733507
27	.0384615	7.00962	7.02000	.00147929	.0729000
28	.0370370	7.25926	7.26923	.00137174	.0724862
29	.0357143	7.50893	7.51852	.00127781	.0721022
30	.0344828	7.75862	7.76786	.00118906	.0717474
31	.0333333	8.00833	8.01724	.00111111	.0714180
32	.0322258	8.25806	8.26667	.00104058	.0711111
33	.0312500	8.50781	8.51613	.000976563	.0708247
34	.0303030	8.75758	8.76563	.000918274	.0705566
35	.0294118	9.00735	9.01515	.000865062	.0703053
36	.0285714	9.25714	9.26471	.000816326	.0700692
37	.0277778	9.50694	9.51429	.000771606	.0698469
38	.0270270	9.75676	9.76389	.000730440	.0696374
39	.0263158	10.0066	10.0135	.000692521	.0694394
40	.0256410	10.2564	10.2632	.000657462	.0692521
41	.0250000	10.5063	10.5128	.000626000	.0690746
42	.0243902	10.7561	10.7625	.000594884	.0689063
43	.0238095	11.0060	11.0122	.000564893	.0687465
44	.0232558	11.2558	11.2619	.000535083	.0685941
45	.0227273	11.5057	11.5116	.000505152	.0684492
46	.0222222	11.7556	11.7614	.000475382	.0683110
47	.0217391	12.0054	12.0111	.000445790	.0681790
48	.0212766	12.2553	12.2609	.000416494	.0680527
49	.0208333	12.5052	12.5106	.000387402	.0679323
50	.0204082	12.7551	12.7604	.000358493	.0678168